

流体: ~~粘滞系数~~  $gh_1 + \frac{P_1}{\rho} + \frac{u_1^2}{2} + h_e = gh_2 + \frac{P_2}{\rho} + \frac{u_2^2}{2} + h_f$ .

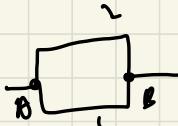
粘滞系数:  $\tau = \mu \frac{du}{dy}$

湍流:  $Re = \frac{\rho u^2}{\mu u/d} = \frac{du/dy}{\mu}$   $Re < 2000 P_{in} \cdot \bar{u} = \frac{1}{2} \rho u^2$   
 $Re > 4000$  滴

$ohf = \lambda \frac{L}{d} \frac{u^2}{2}$   $\left\{ \begin{array}{l} P_{in}: \lambda = \frac{64}{Re} \\ \text{湍流: } \lambda = \left( \frac{L}{d} + 2.5 \right) \frac{u^2}{2} \end{array} \right.$  局阻力:  $h_f = \lambda \frac{u^2}{2}$ .

$\lambda \approx 0.5$ .

串并联:

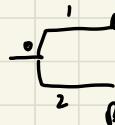


$$H_{tot} = H_{10} + \sum f_1$$

or

$$H_{tot} = H_{10} + \sum f_1$$

$$\sum f_1 = \sum H_{f1}$$



$$H_{tot} + \sum H_{f1} = F_{10} + \bar{B} H_{f2} = H_{tot}$$

扬程:

扬程: ~~能升高的高度~~ “灌注”, 通过灌注灌水

h

$$Pe = \frac{H \rho g}{\eta} : = \rho_v \cdot \rho g H$$

$$\frac{Pe}{\eta} \rightarrow P.$$

扬程增加 - 高度增加  
 $(NPSH)_c =$  No, Li “灌注” 30

$$P_1 / \rho g + \frac{u^2}{2g} - \frac{P_v}{\rho g} = H_{Pen.}$$

傳熱：

Tourier 理論：(2 端條件...)

$$dQ = -\lambda A \frac{dx}{dn}$$

$$q = \frac{dQ}{dx} = -\lambda \frac{dx}{dn}$$

$$R = \frac{L}{K} = \frac{\Sigma x}{\Sigma R} \propto \frac{b_i}{\lambda A} \xrightarrow{\substack{\rightarrow L \\ \downarrow \\ \text{傳熱} \\ \text{面積} \text{ 乘} \text{ 厚度}}}$$

2 端條件

$$Q = \lambda A (T - T_w) \quad \lambda \equiv \frac{\lambda}{b}$$

圓管 B:  $R = \frac{b}{2\pi \lambda m}$

$$\frac{\ln(r_2/r_1)}{2\pi \lambda L}$$

量關係：

$$4 \times \frac{\text{傳熱}}{\text{面積} \times \text{厚度}}$$

對/半圓管的傳熱溫差  $\Delta T_m$ :

$$\frac{\Delta T_b - \Delta T_w}{\ln(\frac{r_2}{r_1})}$$

總傳熱系數：

$$R = \frac{1}{K} = \frac{A}{\lambda_1 A_1} + R_{s1} \frac{A}{A_1} + \frac{b}{\lambda} \frac{A}{A_m} + R_{s2} \frac{A}{A_2} + \frac{A}{\lambda_2 A_2}$$

→ 管“直率” ;  $K = \lambda$

\* 吉布斯  $\rightarrow R_{\text{吉布斯}}$

$$Y_A = \frac{P_A}{P} = \frac{P_A^* T_B}{P_A^* P_B} \Rightarrow x_A = \frac{P - P_B^*}{P_A^* - P_B^*}$$

D<sub>吉布斯</sub> DL.

$$V_A = \frac{P_A}{x_A}$$

$$\propto \frac{V_A}{V_B} \approx \frac{P_A^*}{P_B^*}$$

$$\text{推导: } P_A = T_A^* x_A$$

$T_A$   $\nearrow$ : 正偏

$x_A < 1$ : 逸散

Tränen: Gleichung:  $88 T_B$

$$\lg \alpha = - 9.178 \left[ \frac{(T_B)_0 - (T_B)_B}{(T_B)_0 + (T_B)_B} \right]$$

$\text{或 } T_B \frac{T_B + T_B}{2}$

物料衡算:  $q_{\text{总}} = q_{\text{进料}} + q_{\text{产品}} \quad (1)$   $q_{\text{产品}} x_f = q_{\text{进料}} x_A + q_{\text{产品}} x_m$

操作条件:

解 6:  $y = \frac{R}{R_f} x + \frac{x_f}{R_f}$ ,  $R = \frac{q_f}{q_{fd}}$

解 6:  $y_{nm} = \frac{q'_{nm} x_n}{q'_{nm} - q'_{nm,w}} = \frac{q'_{nm} x_n}{q'_{nm} q_{nm,w}}$

$q$  线:  $y = \frac{q}{q-1} x - \frac{x_f}{q-1}$

$$y = \frac{dx}{1 + (d-1)x}$$

- $q > 1$ :  $x_f$
- $q = 1$ :  $V_B$
- $0 < q < 1$ : 溶液部分互溶
- $q = 0$ : 饱和蒸气
- $q < 0$ : 过热蒸气

插板法 (红字), 原理:  $\frac{\text{实际产量}}{\text{最适产能}} \times 100\%$

$$F_{\text{act}} = \frac{y_n - y_{n+1}}{y_n - y_{n+1}}$$

$$F_{\text{act}} = \frac{x_n - x_m}{x_n - x_m}$$

$$y = \frac{\alpha x}{1 + (\alpha - 1)x}$$

适合生产饱和!!

$$y_i = \gamma d_i$$

① 常见反应器类型:

② 反应速率: 滞后反应器的限制  
中等速率  $\downarrow$   $\rightarrow$  快速速率

计算7: 新鲜空气 T. 作业

$R_{\text{min}}$  相等, 特点, 优点.  
反应速率  $\xrightarrow{\text{平衡}}$  ✓

TR $\eta$ : Murphree 效率

TR $\eta$ : 大机会, 红色湿润

反应器设计: 1. 2. 3.

大-快 —— 小-慢!

化学计算题?

↓  
你会用?

④ 形状因子: 定义,  
物理意义?

圆周, 空间:

反刍运动  
P+

ideal 球型: 球-空间 选择  
选择

3/4 球型:

球型:  $\pi r^2$   $\rightarrow$  经典形状因子的球型

球形 CSTR

更精确地。

Lab 温度

示例:  $C(t) \rightarrow b(t)$

$F_{\text{av}}^2$

$\star \sigma_0^2 \longrightarrow \sigma_p^2$

③  $\sigma_0^2$  的意义: “状态” $\sigma_p^2$   $\in N^{\infty}$  (无限)

$$F = 1 - e^{-\sigma_0^2} \quad \sigma_0^2$$

$$\sigma_0^2 = \frac{2}{Pe} = 1, QH_2$$

$\sigma_0^2 \equiv \sigma_p^2, \sigma_0 \infty$

$$Pe = \frac{uL}{D_0} \Rightarrow \infty$$

$\sigma_0^2 \approx 1$   
HSL  $\downarrow$   
精确度。

分子热力学

7, 3, 内, 51.  $\rho_a$   
 $\downarrow$   
 $\phi_a?$

等价:  $\begin{cases} \text{分子} \\ \text{分子/摩尔} \\ \text{密度(摩尔)} \end{cases}$

$$\text{m/s} \leftarrow v \rightarrow \omega/\text{s}$$
$$-r_a dV = \frac{dN_a}{de}.$$

↓

$$-r_a dv = n_{av} \frac{dn_{av}}{de} \Rightarrow = q_{n_{av}} dx_a$$

$$v = \int_{0}^{x_a} \frac{dn_{av}}{-r_a v} dx_a$$

$$V = q_{n_{av}} \int_{0}^{x_a} \frac{dx_a}{-r_a}$$

$$Z = \frac{V}{q_{n_{av}}} = C_a \int \dots$$

$$\bar{E} = \frac{V}{q_W} = \frac{Z \cdot q_W}{q_W} = q_{vo} C_0 \int \frac{dq_W}{-r_W q_W}$$