

Introduction to the Controlled

thermal Fusion



2.6 To test the sensitivity of the nuclear force model to the shape of the binding energy curve, repeat the derivation of Eq. (2.27) using the following central force:

$$\mathbf{F}_{j}^{(\mathrm{N})} = -\frac{1}{4\pi\varepsilon_{0}r_{\mathrm{c}}^{2}}\mathrm{cosech}^{2}\left(\frac{r^{2}}{r_{\mathrm{c}}^{2}}\right)\mathbf{e}_{R}.$$

As in the text write $r_c = kr_0$ and adjust k so that the maximum of the binding energy curve occurs for iron. This will probably involve a numerical calculation. Compare the result with the one obtained in the text.

$$F_{R}^{(N)} = -F_{0} \frac{k^{2}A}{(A^{1/3} + 1)^{2}(2A^{1/3} + 1)}.$$

$$F_{R}^{(C)} \equiv F_{R}^{(C)} \mathbf{e}_{R} = \frac{F_{0}}{2} \frac{A}{(A^{1/3} + 1)^{2}} \mathbf{e}_{R},$$
(2.27)
(2.25)



$$F_{R}^{(N)} = \frac{1}{4\pi\epsilon_{0}r_{c}^{2}}\frac{3}{4\pi r_{0}^{3}}\int_{V} cosech^{2}\left(\frac{r^{2}}{r_{c}^{2}}\right)cos\alpha d\vec{r}\,\overline{e_{R}} \sim \frac{1}{k^{2}}\int_{r_{0}}^{A^{1/3}r_{0}}cosech^{2}\left(\frac{r^{2}}{r_{c}^{2}}\right)cos\alpha r^{2}d\vec{r}$$





3.3 The purpose of this problem is to investigate the effect of plasma profiles on the alpha power density. The idea behind the calculation is to replace the 0-D model where all

quantities are equal to their average value by a volume-averaged 1-D model where the density and temperature have known profiles that vary in space. Specifically, in a plasma with a circular cross section the volume-averaged alpha power density is defined as

$$\overline{S}_{\alpha} = \frac{2}{a^2} \int_0^a \left(\frac{E_{\alpha}}{4} n^2 \langle \sigma v \rangle \right) r \, \mathrm{d}r.$$

Assume now that the density and temperature profiles are given by

$$n = (1 + \nu_n)\overline{n}(1 - r^2/a^2)^{\nu_n},$$

$$T = (1 + \nu_T)\overline{T}(1 - r^2/a^2)^{\nu_T},$$

where \overline{n} and \overline{T} are the volume-averaged density and temperature respectively. To determine the effect of temperature profile on alpha power density numerically evaluate \overline{S}_{α} for $\nu_n = 0$ and $0 \le \nu_T \le 4$ using $\langle \sigma v \rangle$ from Problem 3.1. For each ν_T find the optimum value of \overline{T} that maximizes \overline{S}_{α} at fixed average pressure: $\overline{p} = 2 [(1 + \nu_n)(1 + \nu_T)/(1 + \nu_n + \nu_T)] \overline{nT} = \text{const.}$ Plot the optimum $\overline{T}(\text{keV})$ and corresponding $\overline{S}_{\alpha}/\overline{p}^2 \equiv C_p$ as a function of ν_T showing the 0-D limit $\nu_n = \nu_T = 0$ for reference. To determine the variation of \overline{S}_{α} with density repeat the above calculation for $\nu_T = 2$ and $0 \le \nu_n \le 4$. Are peaked profiles good, bad, or unimportant in maximizing \overline{S}_{α} ?



fusion reaction rate

$\langle \sigma v \rangle = 10^{-6} \exp\left(\frac{a_{-1}}{T_{i}^{\alpha}} + a_{0} + a_{1}T_{i} + a_{2}T_{i}^{2} + a_{3}T_{i}^{3} + a_{4}T_{i}^{4}\right) m^{3}/s,$						
where $T_i = T_i$ (keV) and				[Nuclear Fusion, 17, 873]		
α	a_{-1}	a_0	a_1	<i>a</i> ₂	<i>a</i> ₃	<i>a</i> ₄
0.2935	-21.38	-25.20	-7.101×10^{-2}	1.938×10^{-4}	4.925×10^{-6}	-3.984×10^{-8}



Homework 3.3. the effect of temperature profile

 $n = (1 + \nu_n)\overline{n}(1 - r^2/a^2)^{\nu_n},$ $T = (1 + \nu_T)\overline{T}(1 - r^2/a^2)^{\nu_T},$

nu_n=0, constant density profile



By Homework 3.3. the effect of temperature profile

Peaked Ti profile leads to high alpha power, however, extremum exists.



Homework 3.3. the effect of density profile





Begin Lomework 3.3. the effect of density profile

Peaked density profile leads to monotonic alpha power

increase





- 4.1 This problem involves the derivation of a generalized version of the Lawson criterion. Consider a subignited reactor in which S_α < S_κ. In the plasma power balance include alpha heating, external heating, and thermal conduction losses. Also, include the power produced by breeding tritium from Li⁶. However, assume that of the total alpha power only a fraction *f* deposits its energy in the plasma while 1 − *f* is immediately lost to the first wall and converted to heat. Assume a thermal conversion efficiency η_t and an input electricity to plasma heating conversion efficiency η_h (i.e., η_h = η_e, η_a = 1).
 (a) Derive an expression for pτ_E = G(Q_E, f) for steady state operation.
 - (b) Assume T = 15 keV, $\eta_t = 0.35$, $\eta_h = 0.5$. Plot curves of $p\tau_E$ vs. Q_E for f = 0, 0.5, 1. Compare the required $p\tau_E$ values at $Q_E = 20$ with the fully ignited value $(Q_E = \infty, f = 1)$ and the Lawson breakeven criterion $(Q_E = 1, f = 0)$.

Homework 4.1

Prove Pout =
$$\left[\leq_{n} + \leq_{Li} + \leq_{B} + \leq_{M} + (l-f) \leq_{A} \right] f_{t}$$
. $(f_{e} = 0.4. + (l-f) q_{e} P_{in}^{(F)})$
 $p_{n}^{E} = \leq_{h}$.
 $f_{n}^{E} = \leq_{h}$.
 $f_{n}^{E} = \int_{A} + \int_{A} + \int_{A} = \int_{A} + \int_{A}$

Homework 4.1

$$\begin{split} & E_{h} = 14 \mid M_{eV} \quad S_{Li} = 4.8 \ M_{eV} \quad S_{a} = 3.5 \ M_{eV} \quad \frac{S_{h} + S_{Li}}{S_{a}} = \beta S_{a} \quad \beta = 5.4 \\ \hline 1 + 1 e S_{e} + 1 f \quad \frac{S_{a}}{12} \quad \frac{P}{12} \quad \frac{S_{a}}{12} \quad \frac{P}{Q_{E} + 1} \quad \frac{S_{a}}{Q_{E} + 1} \quad \frac{P}{Q_{E} + 1} \quad \frac{S_{a}}{S_{a}} = \beta S_{a} \quad \beta = 5.4 \\ \hline \frac{1 + 1 e}{Q_{E} + 1} \quad \frac{S_{a}}{S_{a}} \quad \frac{P}{P} \quad \frac{S_{a}}{S_{a}} = (1 - \frac{1 + 1 e}{Q_{E} + 1}) \quad S_{a} \quad \frac{1 + 1 e}{Q_{E} + 1} \quad S_{a} \quad \frac{S_{a}}{S_{a}} = (1 - \frac{1 + 1 e}{Q_{E} + 1}) \quad S_{a} \quad \frac{S_{a}}{S_{a}} = (1 - \frac{1 + 1 e}{Q_{E} + 1}) \quad S_{a} \quad \frac{S_{a}}{S_{a}} \quad \frac{S_{a}}{S_{a}} = (1 - \frac{1 + 1 e}{Q_{E} + 1}) \quad S_{a} \quad \frac{S_{a}}{S_{a}} \quad \frac{S_{a}}{S_{a}} = (1 - \frac{1 + 1 e}{Q_{E} + 1}) \quad S_{a} \quad \frac{S_{a}}{S_{a}} \quad \frac{S_{a}}{S_{a}} = (1 - \frac{1 + 1 e}{Q_{E} + 1}) \quad S_{a} \quad \frac{S_{a}}{S_{a}} = (1 - \frac{1 + 1 e}{Q_{E} + 1}) \quad S_{a} \quad \frac{S_{a}}{S_{a}} \quad \frac{S_{a}}{S_{a}} = (1 - \frac{1 + 1 e}{Q_{E} + 1}) \quad S_{a} \quad \frac{S_{a}}{S_{a}} \quad \frac{S_{a}}{S_{a}} = (1 - \frac{1 + 1 e}{Q_{E} + 1}) \quad S_{a} \quad \frac{S_{a}}{S_{a}} = (1 - \frac{1 + 1 e}{Q_{E} + 1}) \quad S_{a} \quad \frac{S_{a}}{S_{a}} = (1 - \frac{1 + 1 e}{Q_{E} + 1}) \quad S_{a} \quad \frac{S_{a}}{S_{a}} = (1 - \frac{1 + 1 e}{Q_{E} + 1}) \quad S_{a} \quad \frac{S_{a}}{S_{a}} = (1 - \frac{1 + 1 e}{Q_{E} + 1}) \quad S_{a} \quad \frac{S_{a}}{S_{a}} = (1 - \frac{1 + 1 e}{Q_{E} + 1}) \quad S_{a} \quad \frac{S_{a}}{S_{a}} = (1 - \frac{1 + 1 e}{Q_{E} + 1}) \quad S_{a} \quad \frac{S_{a}}{S_{a}} = (1 - \frac{1 + 1 e}{Q_{E} + 1}) \quad S_{a} \quad \frac{S_{a}}{S_{a}} = (1 - \frac{1 + 1 e}{Q_{E} + 1}) \quad S_{a} \quad S_{$$

 $p au_E$ increases linearly along with the engineering energy gain factor Q_E No alpha heating power, the self-sustained plasma completely depends on the external heating

Best Homework 4.1



$p au_E\,$ increases rapidly in the regime $Q_E < 20\,$

Best Homework 4.1

Increased alpha heating power facilitates the achieve of the self-sustained burning plasma $Q_E \sim \infty$, because the only perturbation comes from thermal conduction losses and the bremsstrahlung is not considered, which is proportion to n^2 sqrt(T)





8.6 A plasma has a constant uniform magnetic field $\mathbf{B} = B_0 \mathbf{e}_z$. Superimposed is an electrostatic electric field of the form $\mathbf{E} = E_0 \cos(\omega t - kz)\mathbf{e}_z$, where ω and k are known constants. Assume a positively charged particle is initially located at z(0) = 0 with a parallel velocity $v_z(0) = v_{\parallel}$. Show that for a sufficiently large value of E_0 the particle is trapped in the wave. Calculate the critical E_0 .



$$\frac{1}{2}mV_z^2 < q \int_0^{\pi/2k} E\cos(\omega t - kz) dz$$

$$V_z < \sqrt{\frac{2qE_0}{m} + \frac{w}{k}}$$

$$E_0 > \frac{m(V_z - \omega/k)^2}{2q}$$



8.13 A positive ion is placed in a sheared magnetic field given by

$$\mathbf{B} = B_0[\mathbf{e}_z + (x/L)\mathbf{e}_y].$$

- (a) Write down the exact equations of motion describing the orbit of the particle.
- (b) Find a relation between $v_z(t)$ and x(t) assuming the following initial conditions: $v_y(0) = v_z(0) = x(0) = y(0) = z(0) = 0$ and $v_x(0) = v_0$.
- (c) Using this relation derive a single, second order ODE for x(t).
- (d) Calculate the x location of the turning point of the orbit.



 $\frac{d^2x}{dt^2} + \omega_c^2 \left(x + \frac{x^3}{2L^2} \right) = 0$

c)

 $\frac{d^2z}{dt^2} = \omega_c \frac{dx x}{dt L}$

 $\omega_c = \frac{qB_0}{m}$

 $V_y^2 + V_z^2 = V_0^2$

From b)

 $x^4 + 4L^2 x^2 - \frac{4L^2 V_0^2}{\omega_c^2} = 0$

- 11.8 A straight 2-D non-circular plasma has an elliptic cross section with horizontal width 2*a* and vertical height $2\kappa a$, where κ is the elongation. The plasma is surrounded by a close fitting circular wall of radius $r = 2\kappa b$ with $b \approx a$. For simplicity assume the "toroidal" field $B_z = B_0 = \text{const.}$ Now, note that the requirement $\nabla \cdot \mathbf{B} = 0$ implies that the magnetic field in the plasma can be written as $\mathbf{B} = \nabla A \times \mathbf{e}_z + B_0 \mathbf{e}_z$, where $A(r, \theta)$ is the vector potential.
 - (a) Using the MHD equilibrium equations and Maxwell's equations show that p = p(A) and derive the partial differential equation satisfied by A.
 - (b) Solve the equation for A assuming that $\mu_0 p(A) = (C^2/2)(A_{\text{max}}^2 A^2)$, where C and A_{max} are constants. To obtain an analytic solution assume that $C\kappa a \ll 1$ and solve by expansion.
 - (c) Magnetic measurements on the wall surface indicate that $B_{\theta}(\kappa a, \theta) = (\mu_0 I / 2\pi \kappa a)(1 + \alpha \cos 2\theta)$, where *I* and α are measured constants. Solve the equation for *A* in the vacuum region between the wall and the plasma (where p = 0). Match the solutions across the plasma–vacuum interface and derive an expression for $\kappa = \kappa(\alpha)$.

(a). $\nabla P \cdot B = B(J \times B) = 0$ $\Rightarrow \nabla p \cdot B = \nabla p \cdot (\nabla A \times \hat{z} + B_0 \hat{z})$ = op. (VAx2) + op(Bo2) p.2=0 ≥ Z. (OP× VA)=0 P5A面平行. > P= P(A) OP=JXB= Juo(OXB)XB =). MODE TX (DAXZ + BOZ) XB JZ=0 = [Ox(VAXZ)]×B : (ZXIJAXZ) = JA(VZ) - (A) - (Z. A) ZZ + (Z. A) ZA - (V. VA)Z = - D'AZ Lo $\mu_0 \nabla p = (- \nabla A \hat{z}) \times \hat{B} = (- \partial A \hat{z}) \times (\nabla A \times \hat{z} + \hat{B}_0 \hat{z})$ = (- JAZ)X(JAXZ) = - JA [=x (OAx=)] = - JA IVA(Z.Z) - Z(Z.ZA)] 部: hop=- v2A vA, A=A(r,o).

(b). 房庭 植位型. (r, b, z).

$$\mu_0 \nabla P / \sigma_A = - \nabla^2 A$$

 $\Rightarrow \mu_0 \frac{dP}{dA} = -\nabla^2 A$, $\mu_0 P(A) = \stackrel{C^2}{=} (A_m^2 - A^2)$
 $\Rightarrow \nabla^2 A + C^2 A = D.$
 $\Rightarrow \frac{3^2 A}{3^{12}} + \frac{3^2 A}{7^{32}} + \frac{5^2 A}{7^{32}} + C^2 A = 0$
对A 3 家友皇 $A(r, b) = R(r) \Phi(b)$
 $\Rightarrow . S \phi \frac{d\Phi}{dB} = -m^2$
 $I \stackrel{C}{=} \frac{d^2 R}{dr^2} + \frac{1}{6} \frac{dR}{dr} + C^2 r^2 - m^2 = 0$
中國解为 $e^{im\theta}$, R为奥家 3 超, 两个条性无关解为观察,
函数 $J_C(Cr)$, Ye CCD, C为所数.

(C). 夏空区沒有电流,成都不成为前从为拉着拉斯分程 JA=0 公底重量重压解为: ALF, B) = S [A] JI(Krs+ BIJ)(Kr) Jeimo 在石麻轴处 1=0, 石麻场有限值, B1=0. 无穷 配处, 1-20. B=0 艺部 减通为0. 取. A= AuJickrs eine r= ka, 6=0. B= 新. 确皇常数 Av值: $= (W) \int \frac{1}{\sqrt{2}} = A_V \frac{2J_1}{2r} + k_{\mu} \qquad I \frac{d}{dr} (rJ_1) = r J_0$ # the BEERE. r=G, BO, Bo, plasma (r=a) = Bo, vacan (r-a)] PAU ANT (F=a) AV=(HA) STING (Jo-Fra) =>. Av = (Hod > that . Ha Jocka - Ji (Ha) 「A - 真定区 ETZ, Ha, B=0, Bo,p= Bo,v J. =>. [=A.p = = A.v] += a. > X= 1- 27[HaJockas-Ji(Kas] Ap MoI Ap= const.



- 11.9 The purpose of this problem is to derive the Grad–Shafranov equation, a famous partial differential equation describing the MHD equilibrium of configurations possessing toroidal symmetry: $Q(R, Z, \phi) \rightarrow Q(R, Z)$.
 - (a) Using $\nabla \cdot \mathbf{B} = 0$ prove that the magnetic field can be written in terms of a flux function $\psi(R, Z)$ as follows: $\mathbf{B} = \nabla \psi \times \mathbf{e}_{\phi}/R + B_{\phi}(R, Z)\mathbf{e}_{\phi}$.
 - (b) From Ampères law derive an expression for $\mu_0 J_{\phi}$ in terms of ψ .
 - (c) From the momentum equation prove that $p(R, Z) = p(\psi)$, where $p(\psi)$ is an arbitrary function.
 - (d) From the momentum equation prove that $B_{\phi}(R, Z) \rightarrow F(\psi)/R$, where $F(\psi)$ is an arbitrary function.
 - (e) From the momentum equation derive the Grad–Shafranov equation:

$$R^2 \nabla \cdot (\nabla \psi/R^2) = -\mu_0 R^2 (dp/d\psi) - F(dF/d\psi).$$

(a).
$$\nabla B = 0 \Rightarrow f = \frac{1}{2} (R R_{R}) + \frac{382}{32} = 0$$
 (
 \overrightarrow{RR} $\overrightarrow{P} = \int B_{Z} - 2\pi R dR \Rightarrow B_{Z} = f \frac{37}{27}$
 $\overrightarrow{R} \nabla B^{=0} : f = \frac{1}{2} (R B_{R}) + \frac{1}{22} (f = \frac{37}{27}) = 0$
 $\Rightarrow B_{R} = -\frac{1}{2} \frac{37}{27}$
 $\overrightarrow{B} = B_{R} \widehat{R} + B_{Z} 2 + B_{Q} \widehat{Q}$
 $= \pi (-\frac{34}{22} \widehat{R} + \frac{27}{27}) + B_{Q} \widehat{Q}$
 $= \nabla \Psi \times \widehat{P} / R + B_{Q} \widehat{Q}$ (R, \overline{Q}, Z) .
(b). $\int J = \nabla X B = \nabla X \left[\frac{\nabla \Psi}{R} \exp \widehat{Q} + B_{Q} \widehat{Q} \right]$
 $= \left(\frac{\widehat{R}}{R} - \widehat{Q} - \frac{2}{27} \right) = 0$
 $= \frac{1}{R} \left[\frac{2(R B_{Q})}{2R} - \frac{2}{2} \frac{(R B_{Q})}{2Z} - \frac{2}{27} \right] - \left[\frac{1}{2} (f + \frac{37}{27}) + \frac{1}{27} \right] \widehat{P}$
 $= -\frac{1}{R} \Delta^{*} \nabla \widehat{Q} + \frac{1}{R} \nabla (R B_{Q}) \times \widehat{Q}$
 $\Delta^{*} \Psi = R \frac{1}{2R} (f + \frac{37}{2R}) + \frac{2^{2}\Psi}{2Z^{2}}$

(c). B.
$$\nabla p = B. (J \times B) = 0$$

 $\Rightarrow B. \nabla p = [\nabla q \times \overline{q} / R + Bq \overline{q}] \cdot \nabla p = 0$
 $\Rightarrow \overline{q} \cdot \nabla q \times \nabla p = 0$
 $\Rightarrow \overline{q} \cdot \nabla p = 0$
 $\Rightarrow p = p(2q).$



(c).
$$\begin{cases} B_{R} = -\frac{1}{R} \frac{2\gamma}{32} \\ B_{P} = \frac{1}{R} \\ B_{Z} = \frac{1}{R} \frac{2\gamma}{3R} \\ T = \frac{1}{R} \frac{1}{R} \frac{2\gamma}{2} \frac{1}{R} \frac{1}{2} \frac{1}{R} \frac{1}{$$

了. マク=0. 由予ア=ア(2).