

3. 约化分布函数

(1) $p^{(1)}(\vec{r}_1)$: Prob density 特定粒子"1"在 \vec{r}_1 而不管其余粒子在何处, 也不管 N 为多少, 一定有 $\int p^{(1)}(\vec{r}_1) d\vec{r}_1 = 1$

已知: $\int P(r^N) d\vec{r}_1 d\vec{r}_2 \dots d\vec{r}_N = 1$

$\Rightarrow p^{(1)}(\vec{r}_1) = \frac{1}{Z_N} \int d\vec{r}_2 d\vec{r}_3 \dots d\vec{r}_N e^{-\beta U(\vec{r}_1; \vec{r}_2, \vec{r}_3 \dots \vec{r}_N)}$
 \vec{r}_1 固定.

* 求 $A(r^N)$ 的平均值.

$\langle A(r^N) \rangle = \frac{1}{Z_N} \int dr^N A(r^N) e^{-\beta U(r^N)}$

eg: $\langle \delta(\vec{r} - \vec{r}_1) \rangle = \frac{1}{Z_N} \int dr^N \delta(\vec{r} - \vec{r}_1) e^{-\beta U(r^N)}$
 $= \frac{1}{Z_N} \int d\vec{r}_2 d\vec{r}_3 \dots d\vec{r}_N e^{-\beta U(\vec{r}; \vec{r}_2 \dots \vec{r}_N)}$
 $= p^{(1)}(\vec{r})$

上式是某个特定的粒子在 \vec{r} 的概率, 可以预见这个 P 是很小的 (1/N), 下面讨论 \vec{r} 处有粒子的概率 (N)

(2) Generalized Distribution Function

$p^{(1)}(\vec{r}) = N p^{(1)}(\vec{r}) = \sum_{i=1}^N \langle \delta(\vec{r} - \vec{r}_i) \rangle \rightarrow \langle \hat{\rho}(\vec{r}) \rangle$

$\rightarrow \int p^{(1)}(\vec{r}) d^3\vec{r} = N$ $\hat{\rho}(\vec{r}) = \sum_{i=1}^N \delta(\vec{r} - \vec{r}_i)$

若 $p^{(1)}(\vec{r}) = \text{const}$, 即粒子均匀分布 $\hat{\rho}(\vec{r})$ 依赖于粒子的构型.

$p^{(1)}(\vec{r}) = \langle \hat{\rho}(\vec{r}) \rangle$

(3) $p^{(2)}(\vec{r}, \vec{r}')$: 有 $\int p^{(2)}(\vec{r}, \vec{r}') d\vec{r} d\vec{r}' = 1$.

(Specific "1" "2") $\Rightarrow p^{(2)}(\vec{r}, \vec{r}') = \frac{1}{Z_N} \int d\vec{r}_3 d\vec{r}_4 \dots d\vec{r}_N e^{-\beta U(\vec{r}, \vec{r}'; \vec{r}_3, \vec{r}_4 \dots \vec{r}_N)}$
 $= \frac{1}{Z_N} \int d\vec{r}_N \int d\vec{r}_2 d\vec{r}_3 \delta(\vec{r} - \vec{r}_1) \delta(\vec{r}' - \vec{r}_2) e^{-\beta U(\vec{r}_1, \vec{r}_2 \dots \vec{r}_N)}$
 $= \langle \delta(\vec{r} - \vec{r}_1) \delta(\vec{r}' - \vec{r}_2) \rangle$

$$\text{那么 } \left\langle \sum_{i=1}^N \sum_{j \neq i}^N \delta(\vec{r}-\vec{r}_i) \delta(\vec{r}'-\vec{r}_j) \right\rangle = N(N-1) \rho^{(2)}(\vec{r}, \vec{r}') \\ \rightarrow \rho^{(2)}(\vec{r}, \vec{r}')$$

$$\int \rho^{(2)}(\vec{r}, \vec{r}') d\vec{r} d\vec{r}' = N(N-1)$$

$$\rho^{(2)}(\vec{r}, \vec{r}') \sim \frac{N(N-1)}{V^2} \sim \rho^2 \quad \rho^{(2)}(\vec{r}, \vec{r}') \text{ 代表 } \vec{r}, \vec{r}' \text{ 的某种关联}$$

$$\text{定义: } g(\vec{r}, \vec{r}') = \frac{\rho^{(2)}(\vec{r}, \vec{r}')}{\rho^2} \quad \rho^{(2)}(\vec{r}, \vec{r}') \text{ 即上面的 } \rho^{(2)}(\vec{r}, \vec{r}')$$

3. 对关联函数.

$$(1) \text{ 定义 } g(\vec{r}, \vec{r}') = \frac{\rho^{(2)}(\vec{r}, \vec{r}')}{\rho^2} \quad \rho^{(2)}(\vec{r}, \vec{r}') = \frac{N(N-1)}{Z_n} \int d\vec{r}_3 \dots d\vec{r}_n e^{-\beta U(\vec{r}, \vec{r}', \vec{r}_3, \dots, \vec{r}_n)}$$

(2) 流体 \rightarrow 平移不变性. 因此 $g(\vec{r}, \vec{r}')$ 应只与相对位置有关

$$\text{即 } g(\vec{r}_1, \vec{r}_2) = g(\vec{r}_1 - \vec{r}_2) \quad \text{记 } \vec{r} = \vec{r}_1 - \vec{r}_2$$

$$\text{则 } g = g(\vec{r})$$

流体 \rightarrow 各向同性. 因此 $g(\vec{r}) = g(r) \rightarrow$ 反映某种径向分布.

(3) 理想气体

$$g(\vec{r}_1, \vec{r}_2) = \frac{\rho^{(2)}(\vec{r}_1, \vec{r}_2)}{\rho^2} \quad Z_n = \int d\vec{r}^n e^{-\beta \times 0} = V^n$$

$$\text{则 } \rho^{(2)}(\vec{r}_1, \vec{r}_2) = \frac{N(N-1)}{V^2} \quad \text{而 } \rho = \frac{N}{V}$$

$$\Rightarrow g(\vec{r}_1, \vec{r}_2) = \frac{N(N-1)}{N^2} \approx 1. = g(r) \quad \text{即 } g(r) = 1 \text{ 表示无关联, 有时引入 } h(r) = g(r) - 1, \text{ 使无关联时 } h(r) = 0.$$

$$(4) \lim_{r \rightarrow \infty} g(r) \rightarrow 1. \text{ (无关联)}$$

$$\lim_{r \rightarrow 0} g(r) \rightarrow 0 \quad (e^{-\beta U} \neq U \rightarrow \infty)$$

$$(5) \rho^2 \int d\vec{r}_1 d\vec{r}_2 g(\vec{r}_1 - \vec{r}_2) = N(N-1)$$

$$\text{利用平移不变性} \rightarrow \rho^2 \int d\vec{r}_2 \left[\int d(\vec{r}_1 - \vec{r}_2) g(\vec{r}_1 - \vec{r}_2) \right] \quad \left[\int d(\vec{r}_1 - \vec{r}_2) g(\vec{r}_1 - \vec{r}_2) \right] \text{ 内的与 } \vec{r}_2 \text{ 无关, } \vec{r}_2 \text{ 可以积分掉.}$$

\downarrow
 $d\vec{r}_2$ 积分得 V .

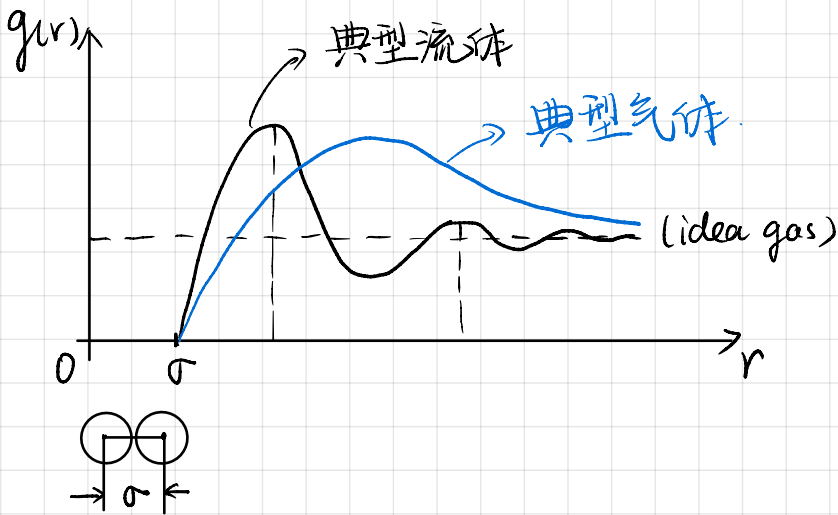
$$= N \rho \int d\vec{r} g(r) \xrightarrow{\text{各向同性}} N \int [p g(r)] 4\pi r^2 dr.$$

代表径向 r 处的密度.

$$\text{则 } N \int [p g(r)] 4\pi r^2 dr = N(N-1)$$

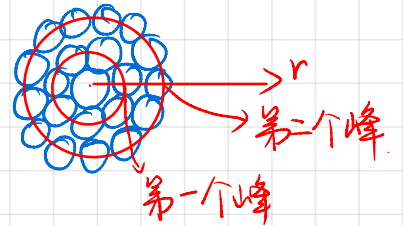
$$\Rightarrow \int d\vec{r} [p g(r)] = N-1 \quad \text{给定一个粒子, 因此为 } N-1$$

$$\rightarrow \int_0^{R_0} (4\pi r^2 dr) [p g(r)] \sim R_0 \text{ 内近邻的粒子数.}$$

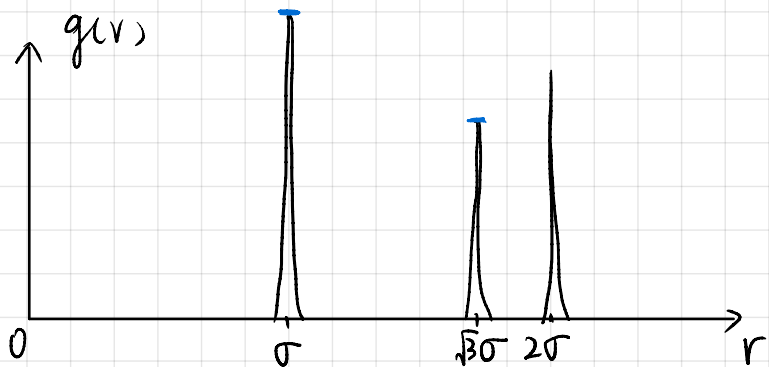
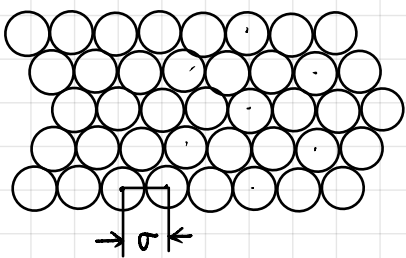


注意峰与谷的位置与流体短程序导致的微观结构有关.

eg:



对固体, 我们也可以定义 $g(r)$ 下面以二维结构为例



注意到 $\int_0^{\sigma+\epsilon} 4\pi r^2 p g(r) dr$ 为最近邻配位数
最近邻 (σ) 与次近邻 ($\sqrt{3}\sigma$) 配位数相同,
但次近邻 r 大, 因此 $g(r)$ 小.

$$(b) \langle \sum_{i \neq j} f(\vec{r}_i, \vec{r}_j) \rangle$$

$$= \frac{1}{Z_N} \int dr^N e^{-\beta U} (\sum_{i \neq j} f(\vec{r}_i, \vec{r}_j))$$

$$= \frac{N(N-1)}{Z_N} \int dr^N e^{-\beta U} f(\vec{r}_1, \vec{r}_2) \quad (N(N-1) \text{ 个})$$

(利用 $\langle f(\vec{r}_1, \vec{r}_2) \rangle = \langle f(\vec{r}_2, \vec{r}_1) \rangle = \dots$)

$$= \int d\vec{r}_1 d\vec{r}_2 f(\vec{r}_1, \vec{r}_2) \times \underbrace{\left[\frac{N(N-1)}{Z_n} \int d\vec{r}_3 \dots d\vec{r}_N e^{-\beta U} \right]} = P^{(2)}(\vec{r}_1, \vec{r}_2)$$

$$= \int d\vec{r}_1 d\vec{r}_2 f(\vec{r}_1, \vec{r}_2) [P^2 g(\vec{r}_1, \vec{r}_2)]$$

* 若 $f(\vec{r}_1, \vec{r}_2) = f(|\vec{r}_1 - \vec{r}_2|) (f(r))$

$$= N \int d\vec{r} f(r) [P g(r)] \xrightarrow{\text{各向同性}} N \int 4\pi r^2 dr f(r) [P g(r)]$$

eg: $\langle \sum_{i \neq j} e^{-i\vec{q} \cdot (\vec{r}_i - \vec{r}_j)} \rangle$

$$= N \int d\vec{r} e^{-i\vec{q} \cdot \vec{r}} [P g(r)]$$

$$= N P \int d\vec{r} e^{-i\vec{q} \cdot \vec{r}} g(r) \quad g(r) \text{ 的 Fourier Transform, 与 X-Ray 衍射的结构因子有关}$$

§.3 热力学性质

1. 内能: $E = \langle K \rangle + \langle U \rangle$

之前分析过, $\langle K \rangle$ 与构型无关, $\langle K \rangle = \frac{\int e^{-\beta U} k d\Gamma}{\int e^{-\beta U} d\Gamma} = \frac{3}{2} NkT$

$$\langle U \rangle = \frac{1}{Z_n} \int e^{-\beta U} U d\Gamma^N$$

* 考察两体势 $U = \frac{1}{2} \sum_{i \neq j} u(|\vec{r}_i - \vec{r}_j|) = \frac{1}{2} \sum_{i \neq j} u(r_{ij})$

$$\langle U \rangle = \frac{1}{2} \sum_{i \neq j} \langle u(r_{ij}) \rangle$$

$$= \frac{1}{2} N \int (4\pi r^2 dr) u(r) [P g(r)]$$

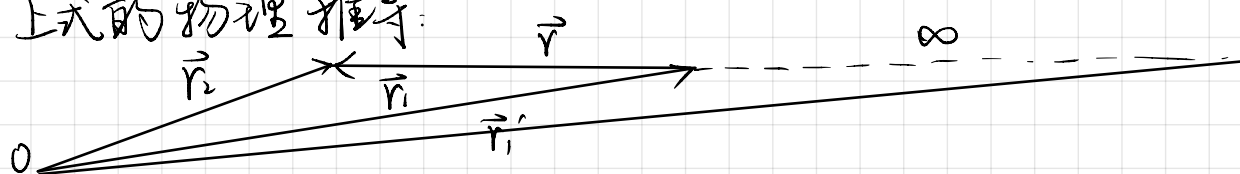
2. 平均力势 (PDF: Potential of Mean Force)

平衡时 $g(r)$ 的起伏可以等效于某种势 (Potential), 下面我们要将

$g(r)$ 与能量联系在一起

(1) $-k_B T \ln g(r) = W(r)$

(2) 上式的物理推导:



固定 \vec{r}_2 , 其余粒子不固定, 有涨落, 将 \vec{r}_1 从 ∞ 远处移到 \vec{r} 处的势能为 $W(r)$, 此时系统 $3 \sim N$ 号粒子自由, \vec{r}_1, \vec{r}_2 固定 (constrained ensemble)

$$\vec{F}_1 = - \frac{\partial}{\partial \vec{r}_1} U$$

$$\begin{aligned} \rightarrow \langle \vec{F}_1 \rangle_{12} &= - \frac{\int d\vec{r}_3 \dots d\vec{r}_N e^{-\beta U} \left(\frac{\partial}{\partial \vec{r}_1} U \right)}{\int d\vec{r}_3 \dots d\vec{r}_N e^{-\beta U}} \quad \text{利用 } \frac{\partial}{\partial \vec{r}_1} (e^{-\beta U}) = -\beta e^{-\beta U} \frac{\partial}{\partial \vec{r}_1} U \\ &= k_B T \frac{\int d\vec{r}_3 \dots d\vec{r}_N \frac{\partial}{\partial \vec{r}_1} (e^{-\beta U})}{\int d\vec{r}_3 \dots d\vec{r}_N e^{-\beta U}} \\ &= k_B T \frac{\partial}{\partial \vec{r}_1} \ln \left(\int d\vec{r}^{N-2} e^{-\beta U} \right) \cdot \left(\frac{N(N-1)}{Z_N} \int d\vec{r}^{N-2} e^{-\beta U} = \rho^{(2)}(\vec{r}_1, \vec{r}_2) \right) \\ &= k_B T \frac{\partial}{\partial \vec{r}_1} \ln \left(\rho^2 g(\vec{r}_1, \vec{r}_2) Z_N / (N(N-1)) \right) \quad = \rho^2 g(\vec{r}_1, \vec{r}_2) \\ &= k_B T \frac{\partial}{\partial \vec{r}_1} \ln g(\vec{r}_1, \vec{r}_2) \quad (\text{只有 } g(\vec{r}_1, \vec{r}_2) \text{ 中含 } \vec{r}_1) \end{aligned}$$

$$W(\infty) - W(r) = \int_{\infty}^{\vec{r}_2 + \vec{r}} \langle \vec{F}_1 \rangle \cdot d\vec{r}_1$$

$$\Rightarrow W(r) = - \int_{\infty}^{\vec{r}_2 + \vec{r}} k_B T \left[\frac{\partial}{\partial \vec{r}_1} \ln g(\vec{r}_1, \vec{r}_2) \right] d\vec{r}_1$$

$$= - k_B T \ln g(\vec{r}_1, \vec{r}_2) \Big|_{\vec{r}_1 = \vec{r}_2 + \infty}^{\vec{r}_1 = \vec{r}_2 + \vec{r}}$$

$$= k_B T \ln \underbrace{g(\vec{r}_2 + \infty, \vec{r}_2)}_{=1} - k_B T \ln \underbrace{g(\vec{r}_2 + \vec{r}, \vec{r}_2)}_{=g(\vec{r}) = g(r)}$$

$$= - k_B T \ln g(r) = W(r)$$

* 稀薄气体 $-k_B T \ln g(r) = U(r)$ (无其余粒子的作用)

3. 压强 (两体势系统 $U = \frac{1}{2} \sum_{i \neq j} u(r_{ij})$)

1) 理想气体 $\beta P = \frac{N}{V} = \rho$, 但存在相互作用时, $\beta P = \rho + B_2(T) \rho^2 + O(\rho^3)$

$B_2(T)$ 称为第二维里系数, 统计力学要找出 $B_2(T)$ 与 $u(r)$ 的关系,

有以下结论: $\beta P = \rho + B_2(T) \rho^2$

$$\rho B_2(T) = - \frac{1}{6 k_B T} \int d\vec{r} \left[\rho g(r) \cdot r \frac{du(r)}{dr} \right]$$

证明思路: $p = -\left(\frac{\partial F}{\partial r}\right)_{N,T}$, 作业 7.11.

(2) $p \ll 1$, $w(r) \sim u(r)$ $g(r) = e^{-\beta w(r)} \approx e^{-\beta u(r)}$

$$B_2(T) = -\frac{\beta}{6} \int \left\{ \left[e^{-\beta u(r)} \frac{du(r)}{dr} \right] r \right\} 4\pi r^2 dr.$$

$$= \frac{1}{6} \int_0^\infty dr \cdot 4\pi r^3 \frac{d}{dr} (e^{-\beta u(r)} + c)$$

$$= \frac{2\pi}{3} r^3 (e^{-\beta u(r)} + c) \Big|_{r=0}^{r=\infty} - \int_0^\infty dr (e^{-\beta u(r)} - c) \frac{d}{dr} \left(\frac{2}{3} \pi r^3 \right)$$

使边界项为 0 $\Rightarrow c = -1$ ★

$$\Rightarrow B_2(T) = - \int_0^\infty dr (2\pi r^2) [e^{-\beta u(r)} - 1]$$

$$= -\frac{1}{2} \int d\vec{r} [e^{-\beta u(r)} - 1] = -\frac{1}{2} \int d\vec{r} f(r)$$

$$(f(r) = e^{-\beta u(r)} - 1) \quad (\text{作业 } 7.12, 7.13, 7.14)$$

证明 p 的表达式:

$$p = -\left(\frac{\partial F}{\partial v}\right)_{N,T} \quad F = -kT \ln Q_{cl} \quad Q_{cl} = \frac{1}{N! \lambda^{3N}} \int d\vec{r}^N e^{-\beta U(\vec{r}^N)}$$

$$\Rightarrow p = \frac{\partial kT \ln Q}{\partial v} \Big|_{N,T} = \frac{kT}{Z_N} \frac{\partial}{\partial v} Z_N$$

$$\frac{\partial}{\partial v} Z_N = \frac{\partial}{\partial v} \int d\vec{r}_1 \dots d\vec{r}_N e^{-\beta U(\vec{r}_1, \dots, \vec{r}_N)}$$

$$\text{令 } x_i = \frac{1}{V^{1/3}} x_i \quad \text{则 } Z_N = V^N \int d\vec{r}'_1 \dots d\vec{r}'_N e^{-\beta U(V^{1/3} \vec{r}'_1, \dots, V^{1/3} \vec{r}'_N)}$$

$\xrightarrow{\text{与 } V \text{ 无关}}$

$$\Rightarrow \frac{\partial}{\partial v} Z_N = \left[\frac{\partial}{\partial v} (V^N) \right] \int d\vec{r}'^N e^{-\beta U(\vec{r}'^N)} + V^N \int d\vec{r}'^N \frac{\partial}{\partial v} e^{-\beta U(\vec{r}'^N)}$$

$$\frac{N}{V} \int d\vec{r}'^N e^{-\beta U(\vec{r}'^N)} = p Z_N$$

$$\frac{\partial}{\partial v} U(\vec{r}'^N) = \frac{1}{2} \sum_{i \neq j} \frac{\partial}{\partial v} u(r_{ij}) = \frac{\partial u(r_{ij})}{\partial r_{ij}} \frac{\partial r_{ij}}{\partial v}$$

$$\text{而 } r_{ij} \propto V^{1/3} \Rightarrow \frac{dr_{ij}}{dv} = \frac{r_{ij}}{3v}$$

则 $\frac{\partial}{\partial V} Z_n$ 中第二项为

$$\begin{aligned} & \int dr^N (-\beta) e^{-\beta U} \left[\frac{1}{2} \sum_{i \neq j} \frac{r_{ij}}{3V} \cdot \frac{\partial U(r_{ij})}{\partial r_{ij}} \right] \\ &= -\frac{\beta}{6V} \int dr^N e^{-\beta U} \left(\sum_{i \neq j} r_{ij} \frac{\partial U_{ij}}{\partial r_{ij}} \right) \\ &= -\frac{\beta}{6V} \int dr^N N(N-1) e^{-\beta U} r_{12} \frac{\partial U(r_{12})}{\partial r_{12}} \\ &= -\frac{\beta}{6V} \int d\vec{r}_1 d\vec{r}_2 r_{12} \frac{\partial U(r_{12})}{\partial r_{12}} \cdot \underbrace{N(N-1) \int dr^{N-2} e^{-\beta U}}_{= Z_n \rho^2 g(\vec{r}_1, \vec{r}_2)} \\ &= -\frac{\beta}{6V} \int d\vec{r}_1 d\vec{r}_2 r_{12} \frac{\partial U(r_{12})}{\partial r_{12}} \rho^2 g(\vec{r}_1, \vec{r}_2) \cdot Z_n \end{aligned}$$

(利用平移不变性 令 $\vec{r}_1 - \vec{r}_2 = \vec{r}$)

$$= -\frac{\beta}{6V} \int d\vec{r}_2 \int d\vec{r} r \frac{\partial U(r)}{\partial r} \rho^2 g(\vec{r}) \cdot Z_n$$

(利用各向同性, $g(\vec{r}) = g(r)$)

$$= -\frac{\beta \rho}{6} \int d\vec{r} [\rho g(r)] r \frac{\partial U(r)}{\partial r} \cdot Z_n = \rho^2 B_2(T) Z_n$$

代回原式

$$P = k_B T \frac{1}{Z_n} \frac{\partial}{\partial V} Z_n = (\rho + B_2(T) \rho^2) k_B T$$

$$\Rightarrow \beta P = \rho + B_2(T) \rho^2$$

4. 化学势 μ $G = F - TS + PV = \mu N$

对于只与构型有关的物理量 $A(r^N)$ $\langle A \rangle = \int A(r^N) e^{-\beta U(r^N)} / Z_n$

这些量统称为力学量. P 也是此类量. (位力定理告诉我们 $P \propto \sum \langle \vec{F}_i \cdot \vec{r}_i \rangle$)

但对于 S , $S \neq S(r^N)$, 即一个构型没有熵, 而是与所有系综有关, 类似于熵这一类的物理量称为热力学量.

$$dF = -SdT - PdV + \mu dN$$

$$\text{当 } N \rightarrow \infty \text{ 时 } \frac{\Delta F}{\Delta N} = F_N - F_{N-1}$$